

IMDD vs Coherent

Will Datacenter be the New Battleground?

Summer Topicals 2020 Virtual Conference

Tutorial TuA2.2 10:45AM – 11:30AM MDT

14 July 2020

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Outline

- **NRZ vs HOM**
- Serial vs WDM
- Coherent in Telecom
- Coherent in Datacom
- IMDD vs Coherent SNR
- Intra Datacenter Optics
- Appendices

Shannon-Hartley Theorem

$$C = B \log_2 (1 + S/N)$$

$C \triangleq$ Channel capacity

$B \triangleq$ Bandwidth

$S \triangleq$ Signal Power

$N \triangleq$ Noise Power

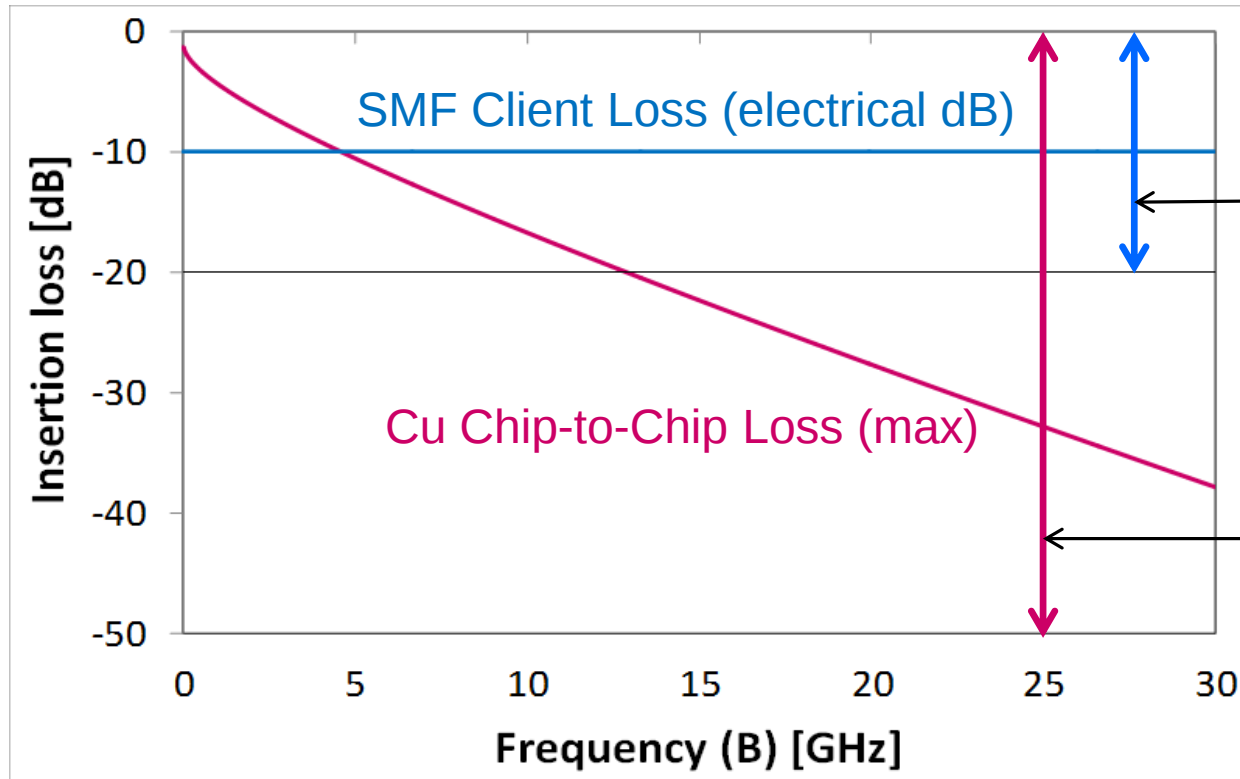
Guidance to increase C:

If B limited, use S/N to increase modulation order

If S/N limited, use B to increase Baud rate

C. Cole, "SMF PMD Modulation Observations", 400 Gb/s Ethernet Task Force, IEEE 802.3 Plenary Session, Berlin, Germany, 10-12 March 2015cc

Cu C2C SerDes & SMF Client TRX S/N (BtB, no FEC)

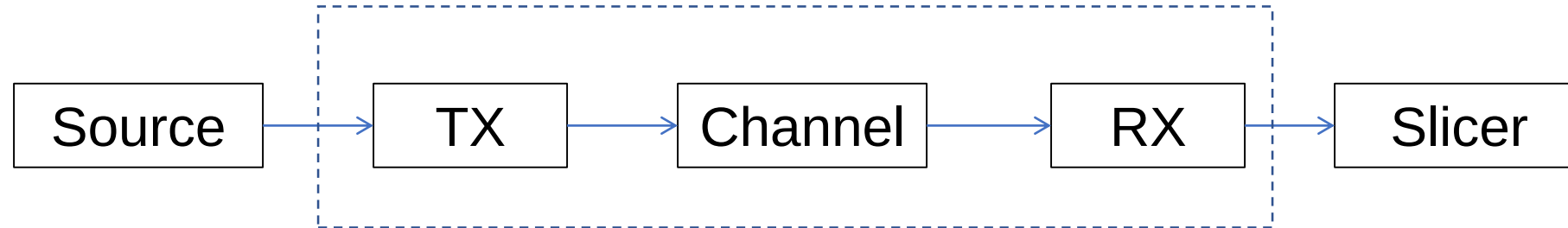


SMF client TRX:
low S/N
high B
Shannon says: use NRZ

Cu C2C SerDes:
high S/N
low B
Shannon says: use HOM

HOM $\triangleq$ Higher Order Modulation

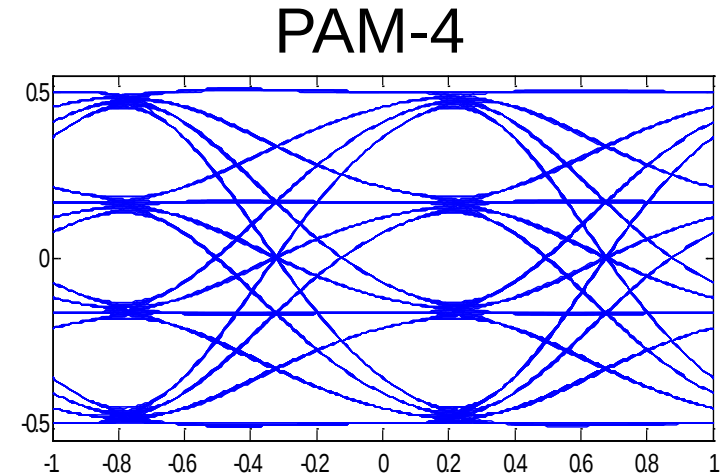
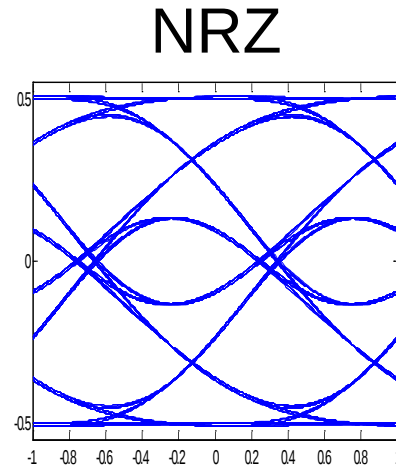
Ideal SMF Client System Model



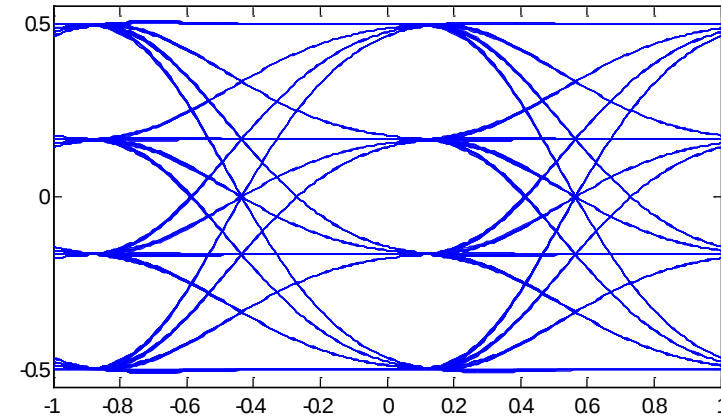
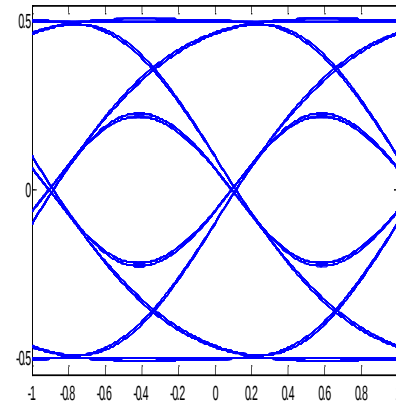
- SMF client channel ideal
- (TX * Channel * RX) modelled as 4th order BT filter
- $B = \alpha$ bit-rate
- Ex. bit rate = 56Gb/s
 - ex. 1: $\alpha = 0.25 \rightarrow B = 14\text{GHz}$
 - ex. 2: $\alpha = 0.30 \rightarrow B = 17\text{GHz}$

Slicer Input Eyes of Ideal Noiseless SMF Client System

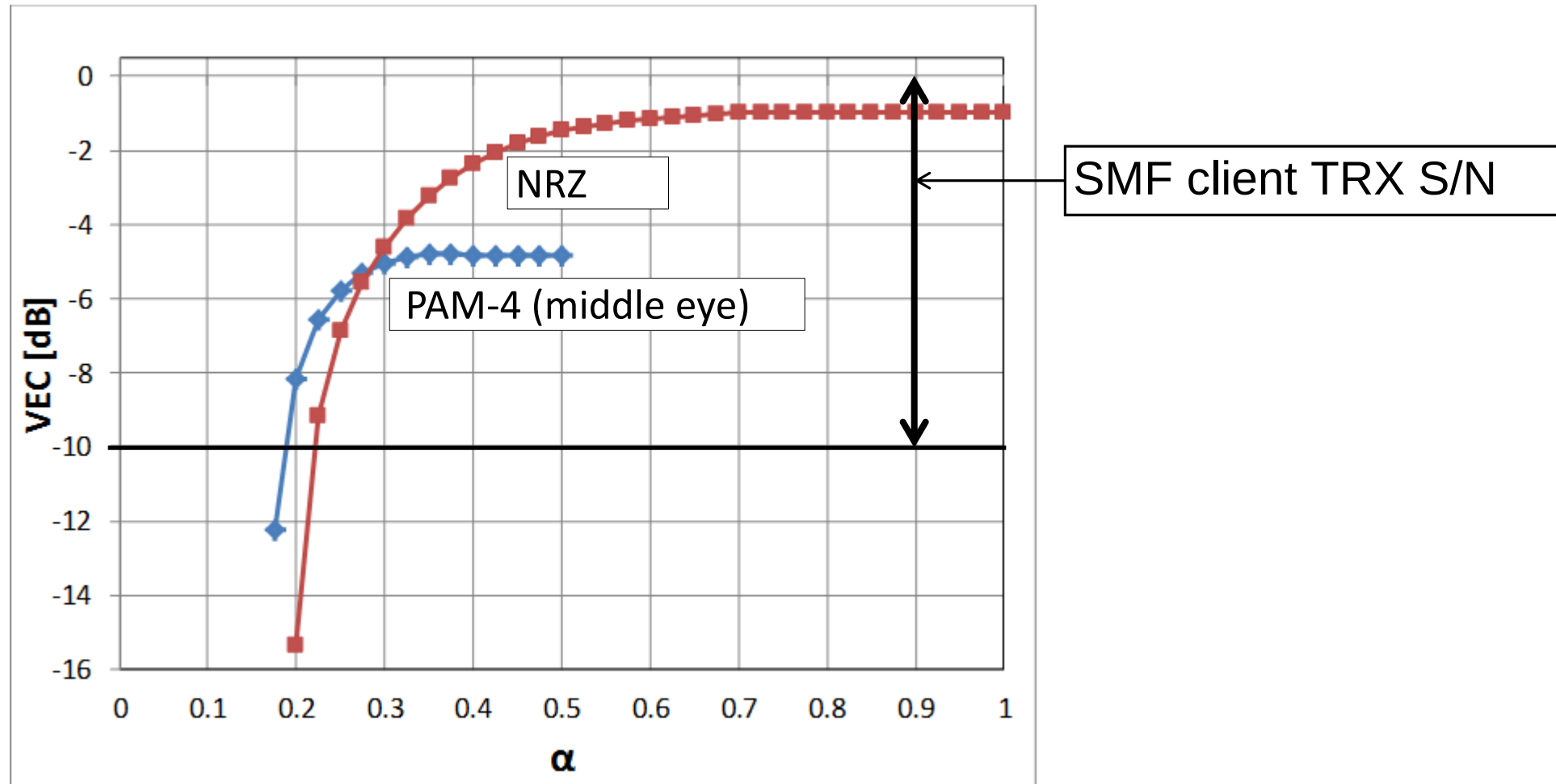
Ex. 1. $\alpha = 0.25$ (14GHz)
NRZ VEC $\approx$ PAM4 VEC



Ex. 2. $\alpha = 0.30$ (17GHz)
NRZ VEC $<$ PAM4 VEC



Vertical Eye Closure at Slicer Input w/ Noise Normalization



IEEE Modulation Choice for 50Gb/s and Faster Rates

- Optics is the tail on the IC industry dog
 - 50G PAM4 ASIC SerDes was first developed for the Cu channel
 - IC Vendors wanted to maximize their ADC and DSP investment
- IC dog wagged the optics tail
 - IEEE ignored Shannon
 - PAM4 standardized for 50G and 100G Ethernet optical lane rates
 - 200G (4x50G PAM4) FR4 will soon ship in the millions
- Optics & electronics today easily support 50G NRZ
 - Extra cost and power of 50G PAM4 ADC, DSP, SNR locked-in forever

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Ethernet Optics History: 1 & 10GbE

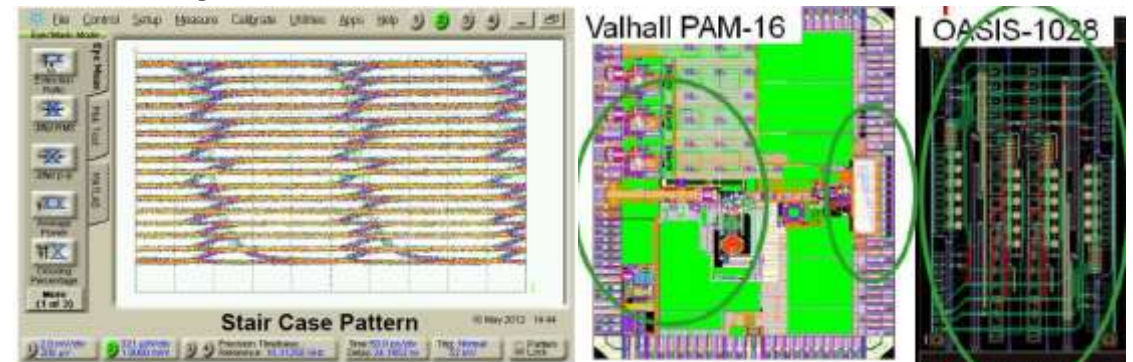
- 1GbE standard adopted in 1998
 - 1 λ Serial NRZ (LX)
 - Shipped in the millions
- 10GbE standard adopted in 2002
 - 4 λ WDM NRZ (LX4)
 - 1 λ Serial NRZ (LR4)
 - 5-year delay in 10GbE adoption after 90's Tech bubble collapse
 - 10GBaud optics & electronics matured to easily support 10G NRZ
- 10G LR4 shipped in the millions
- 10G LX4 became a sad footnote in Ethernet optics history
- “Serial is always cheaper” myth is born

Ethernet Optics History: 40GbE

- 40GbE standard adopted in 2010
 - “Serial is always cheaper” myth well established
 - Fierce debate in the IEEE between:
 - 4λ WDM NRZ (LR4) vs.
 - 1λ Serial NRZ (FR)
 - IEEE split the baby, adopted both
- 40G LR4 shipped in the millions
- 40G FR became a sad footnote in Ethernet optics history

Ethernet Optics History: 100GbE

- 100GbE standard, targeted at the datacenter, adopted in 2015
 - “Serial is always cheaper” myth going strong
 - Fierce debate in the IEEE about duplex SMF spec between:
 - 4λ CWDM NRZ (FR4)
 - 1λ Serial PAM16/8 (FR)
 - IEEE could not reach agreement, and neither was adopted
- 100G CWDM4 spec developed immediately after in an MSA in 6 months
 - Shipped in the millions
- 100G PAM16/8 became a sad footnote in Ethernet optics history
- \$240M SNR math lesson for Cisco



Ethernet Optics History: 400GbE

- 400GbE standard adopted in 2017
 - “Serial is always cheaper” myth unwavering
 - Fierce debate in the IEEE between:
 - $2\lambda \times 50\text{G}$ WDM for 100G FR2 and $8\lambda \times 50\text{G}$ LWDM 400G LR8
 - $1\lambda \times 100\text{G}$ Serial for 100G FR and 400G PSM DR4
 - IEEE split the baby, adopted 400G LR8 and DR4, but no 100G FR2
- 400G $8\lambda \times 50\text{G}$ LWDM LR8 shipped in low volume into early Telecom apps
- 400G $4\lambda \times 100\text{G}$ CWDM FR4 standardized soon afterwards

Ethernet Optics History: 400GbE (2)

- Ethernet optics sad story 1: no Web2.0 deployment of 400GbE
 - Huge industry R&D investment into 1st Gen 400GbE DR4 & FR4 with no ROI
 - 2nd Gen 400GbE will start shipping in volume in 2023 or later when Ethernet switches ship with 100G I/O
- Ethernet optics sad story 2: no low-cost, low-power 2 λ 100GbE optics matched to today's Ethernet switches with 50G I/O, forcing shipment of:
 - 4 λ 100G CWDM4 with 1:2 reverse gearbox (most Web2.0s), or
 - 1 λ 100G FR with 2:1 forward gearbox (Amazon mainly)
 - Either way, significant cost and power added to 100G Ethernet optical links

Outline

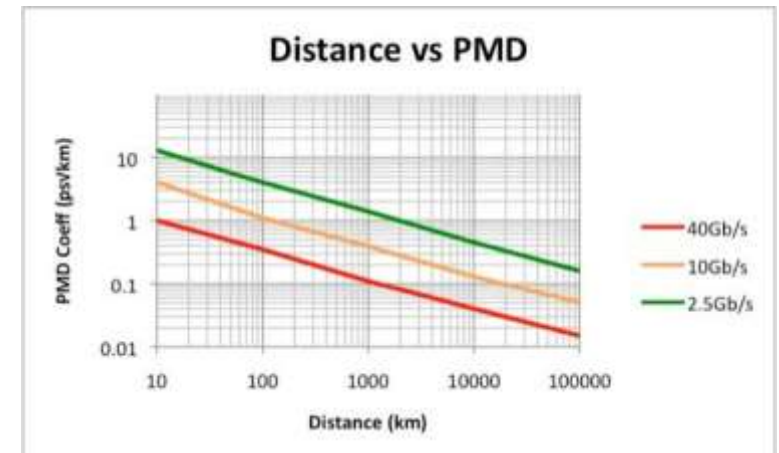
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G.652 SMF DWDM Transport C-band Spec Limits

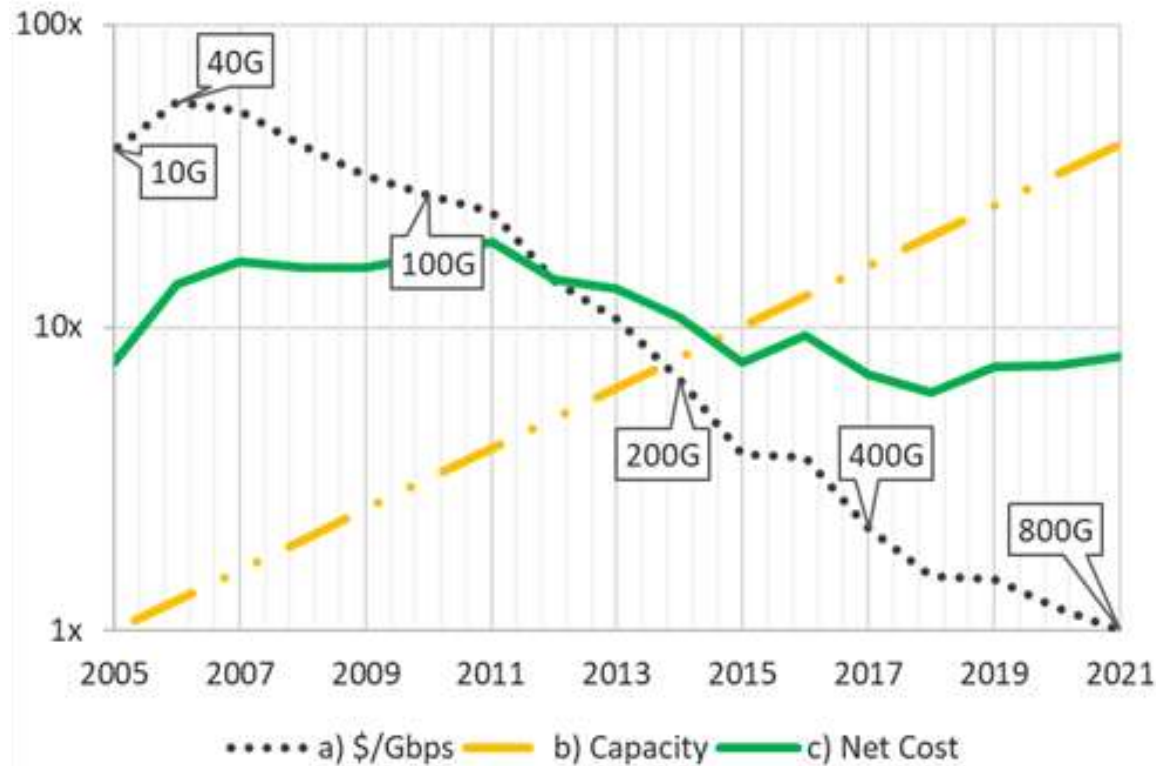
- Loss
 - nom, max: 0.2, 0.28dB/km
 - **IF** link SNR was only determined by link loss
 - Coherent SNR $\approx$ 2x IMDD SNR, in dB
 - Coherent reach $\approx$ 2x IMDD reach, i.e. half the amplifier cost
- Bandwidth (B)
 - Spectral Efficiency is key metric because of fiber deployment cost
 - G.694.1 channel bandwidths: 25 to 100GHz
 - Coherent has 4 orthogonal channels: I, Q, TE, TM
 - Shannon says: If B limited, use S/N to increase modulation order

G.652 SMF DWDM Transport C-band Spec Limits (2)

- Chromatic Dispersion (CD)
 - nom, max: 17, 20ps/nm-km
 - CD penalty variable with link reach
 - IMDD Fixed EQ: unique CDF length for each link
 - Coherent adaptive EQ: common for all links
- Polarization Mode Dispersion Q (PMDQ)
 - A&C nom: $0.5\text{ps}/\sqrt{\text{km}}$
 - B&D nom: $0.2\text{ps}/\sqrt{\text{km}}$
 - DGD is important over long reaches
 - Coherent adaptive EQ tracks polarization



Transport Cost vs Time



10G - 40G: IMDD

100G - 800G: Coherent

“A straight line will continue indefinitely as a straight line”

Optical Networks Forecast: 2018 – 2023, Jan 2019 Representative cost of optical transport capacity over time and transponder generations based on historical average sales price (ASP) of DWDM line card data from Ovum.

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G.652 1km SMF CWDM4 O-band Spec Limits

- Loss
 - max: 0.47dB
 - Connectors and other passives determine link loss
 - Nom link loss budget: 4dB
 - SMF loss is not important
- Bandwidth (B)
 - 4 wavelength band: 10THz
 - 1 wavelength channel: 800GHz
 - Shannon says: If S/N limited, use B to increase Baud rate
 - SMF bandwidth is not important

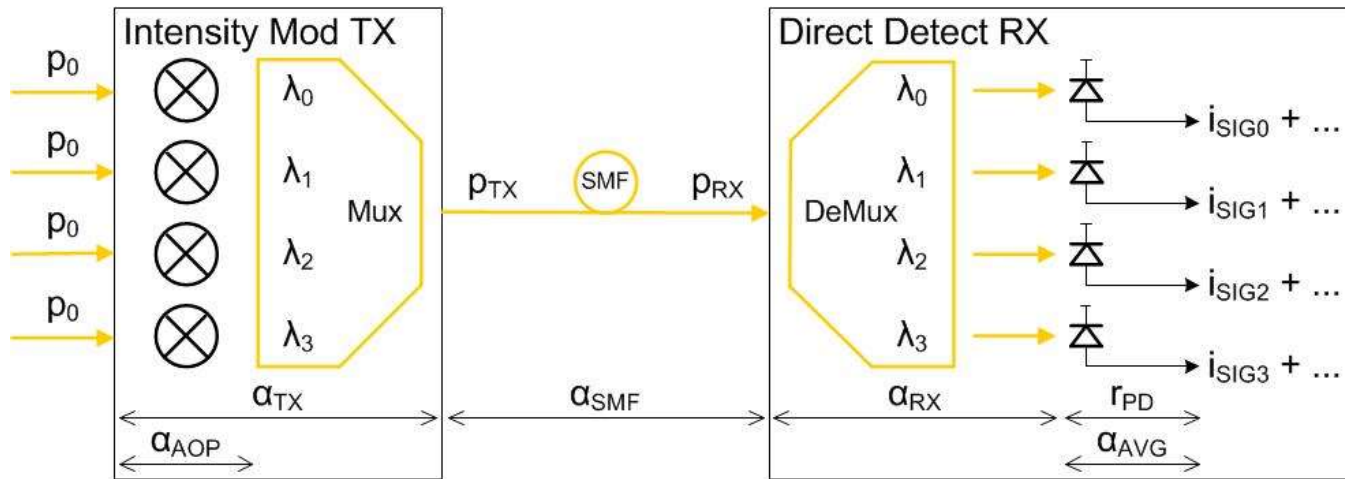
G.652 1km SMF CWDM4 O-band Spec Limits (2)

- Chromatic Dispersion (CD)
 - min: -6ps/nm
 - max: 3ps/nm
 - SMF CD penalty is not important
- Polarization Mode Dispersion Q (PDM_Q)
 - A&C nom: 0.5ps
 - B&D nom: 0.2ps
 - SMF DGD penalty is not important

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Direct Detection (DD) Signal Path



$$p_{\text{IN-TX}} = 4 p_0$$

$$p_{\text{RX}} = \alpha_{\text{SMF}} p_{\text{TX}}$$

$$p_{\text{TX}} = \alpha_{\text{TX}} \alpha_{\text{AOP}} p_{\text{IN-TX}}$$

$$p_{\text{PD}} = \alpha_{\text{RX}} p_{\text{RX}} / 4$$

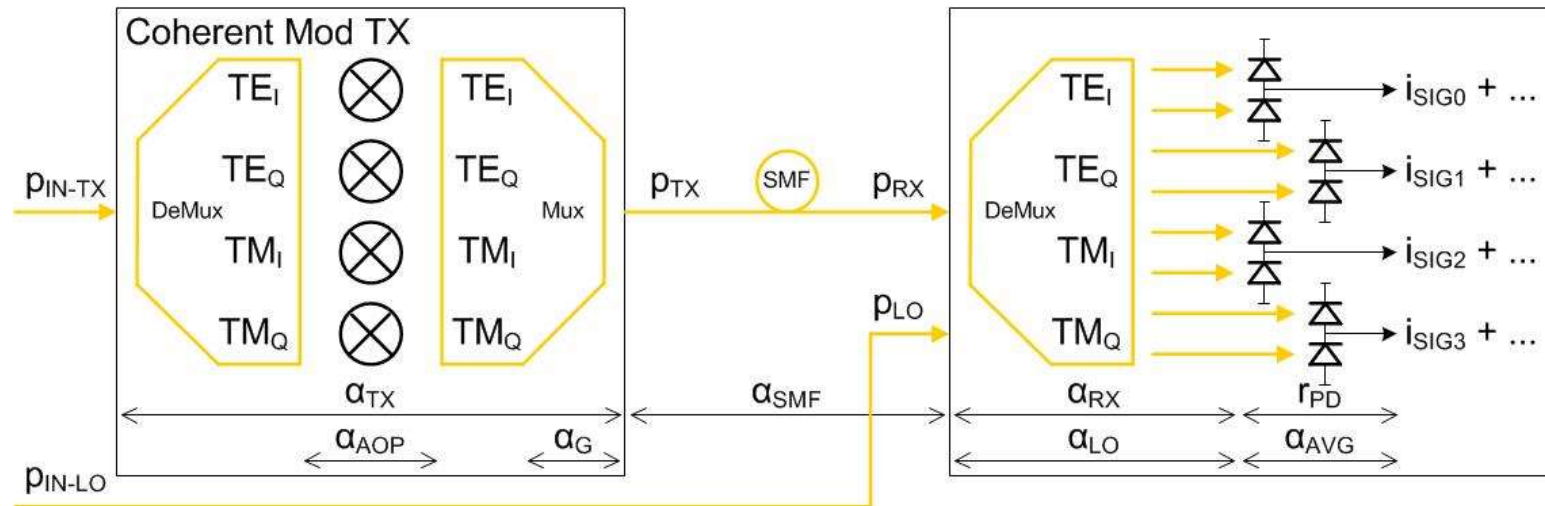
$$i_{\text{SIG}} = \alpha_{\text{AVG}} r_{\text{PD}} p_{\text{PD}}$$

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

$$\sqrt{\text{snr}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{TX}} \alpha_{\text{AOP}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

C. Cole, "Inside the Datacenter is not yet a Nail for the Coherent Hammer", WS05, Data Centers 1, Session 1, ECOC 2018, Rome, Italy, 23 Sep. 2018.

Coherent (CH) Signal Path



$$p_{\text{IN-TX}} = 4 \alpha_{\text{LS}} \alpha_{\text{TEC}} p_0$$

$$p_{\text{TX}} = \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}} p_{\text{IN-TX}}$$

$$p_{\text{IN-LO}} = 4 (1 - \alpha_{\text{LS}}) \alpha_{\text{TEC}} p_0$$

$$i_{\text{SIG}} = \alpha_{\text{AVG}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})} i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

$$\sqrt{\text{snr}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}}) \alpha_{\text{TEC}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})}$$

$$p_{\text{RX}} = \alpha_{\text{SMF}} \alpha_{\text{TX}}$$

$$p_{\text{PD-RX}} = \alpha_{\text{RX}} p_{\text{RX}} / 4$$

$$p_{\text{LO}} = p_{\text{IN-LO}} \quad p_{\text{PD-LO}} = \alpha_{\text{LO}} p_{\text{LO}} / 4$$

$$\text{Optical } \Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} \text{ dB}$$

$A \triangleq$ loss in optical -dB

$$A = -10\log_{10}(\alpha)$$

$$\Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} = 10\log_{10}(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})$$

$$\begin{aligned} \Delta\text{SNR}_{\text{DD-CH}} / 2 = & - (A_{\text{AOP-DD}} + A_{\text{TX-DD}} + A_{\text{SMF}}) \\ & + (A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + A_{\text{SMF}}) / 2 + A_{\text{TEC}} \\ & - (A_{\text{AVG-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}) \\ & + (A_{\text{AVG-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}) \end{aligned}$$

$$A_{\text{TXT-DD}} = A_{\text{AOP-DD}} + A_{\text{TX-DD}} \qquad A_{\text{RXT-DD}} = A_{\text{AVG-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}$$

$$A_{\text{TXT-CH}} = A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + 2A_{\text{TEC}} \qquad A_{\text{RXT-CH}} = A_{\text{AVG-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}$$

$$\Delta\text{SNR}_{\text{DD-CH}} = (A_{\text{TXT-CH}} + A_{\text{SMF}} + 2A_{\text{RXT-CH}}) - 2(A_{\text{TXT-DD}} + A_{\text{SMF}} + A_{\text{RXT-DD}})$$

Optical $\Delta\text{SNR}_{\text{DD-CH}}$ dB Examples

- Equal laser input AOP (TEC ignored):

$$\Delta\text{SNR}_{\text{DD-CH}} = ((A_{\text{TXT-CH}} + A_{\text{SMF}}) - 2(A_{\text{TXT-DD}} + A_{\text{SMF}})) + 2(A_{\text{RXT-CH}} - A_{\text{RXT-DD}})$$

- 100G EML NRZ CWDM4 IMDD vs 100G SiPIC QPSK Coherent

- Ex.1: **4dB** Link Loss (2km, typical intra datacenter)

$$\Delta\text{SNR}_{\text{DD-CH}} = ((17 + 4) - 2(5 + 4)) + 2(4 - 2) = \mathbf{7dB}$$

- Ex.2: **11dB** Link Loss (20km, or 2km & one 7dB loss optical switch)

$$\Delta\text{SNR}_{\text{DD-CH}} = ((17 + 11) - 2(5 + 11)) + 2(4 - 2) = \mathbf{0}$$

- Ex.2: **18dB** Link Loss (40km, or 2km & two 7dB loss optical switches)

$$\Delta\text{SNR}_{\text{DD-CH}} = ((17 + 18) - 2(5 + 18)) + 2(4 - 2) = \mathbf{-7dB}$$

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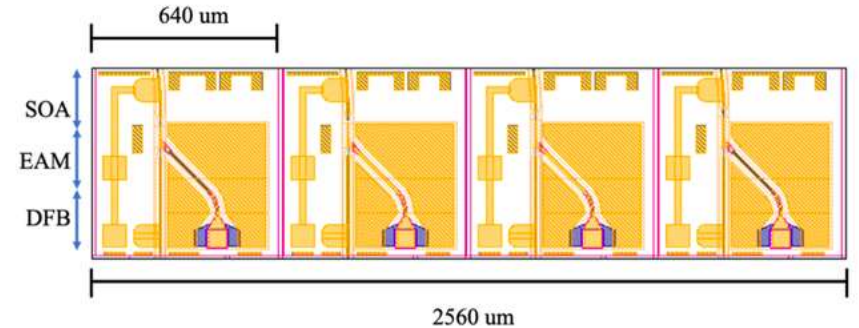
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Intra Datacenter Optics Requirements

- What's important?
 - Cheap laser(s)
 - Cheap SNR (low loss components)
 - Cheap assembly and packaging
 - Cheap testing
- What does Coherent offer?
 - Expensive Laser
 - High loss components
 - Best case comparable packaging cost to IMDD
 - Complex testing

TX Modulator Size Comparison

- IMDD InP EML length:
 - 400 - 500um (EA $\approx$ 120um)
- Coherent Si MZM length:
 - 2 - 4mm
- 4 channel Coherent to IMDD TX area ratio:
 - 10 - 20x



Teriphic project, 4x100G PAM4 EML TX

Intra Datacenter Optics Today: Pluggable

- Characteristics
 - \$1 - \$2/Gb
 - ~30pJ/bit
 - IMDD DML or EML uncooled TX
 - 4λ CWDM NRZ or PAM4
 - Link budget: 4dB
- IMDD vs. Coherent SNR, equal laser DC Power (TEC included):
100G EML NRZ CWDM4 IMDD vs 100G SiPIC QPSK Coherent
 $\Delta\text{SNR}_{\text{DD-CH}} = 11.5\text{dB}$
(same result for PAM4 IMDD vs QAM16 Coherent)

Intra Datacenter Optics Tomorrow: Co-packaged

- Requirements
 - Co-packaged with Ethernet Switch ASIC
 - 256 - 512 data lanes
 - <\$1/Gb
 - <10pJ/bit
 - Link budget: 4dB
- IMDD vs. Coherent SNR, equal laser DC Power (TEC included):
100G SiPIC NRZ CWDM4 IMDD vs 100G SiPIC QPSK Coherent
 $\Delta\text{SNR}_{\text{DD-CH}} = 1.5\text{dB}$
(same result for PAM4 IMDD vs QAM16 Coherent)

Summary

- Coherent advantages in Transport are unimportant in Intra Datacenter
- Coherent indefinitely locks in the cost and power of ADCs and DSPs
 - This is what PAM4 did for >100G Ethernet optics
 - Good for IC vendors, bad for everyone else as optics improve
- “Serial is always cheaper” is a myth for leading data rates
 - 10GbE was the last time it was true
 - 1 λ Coherent is higher cost and power than 4 λ IMDD
- Coherent does not reduce the cost and power of short reach optics
- There is no IMDD vs Coherent competition for Intra Datacenter links
 - Coherent is not even on the battleground

IMDD vs Coherent

Thank You

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Direct Detection (DD) Signal Path Variables

p_0	$\triangleq$ Input POP (Peak Optical Power) reference
$p_{\text{IN-TX}}$	$\triangleq$ TX input POP = AOP (Average OP) if CW
α_{AOP}	$\triangleq$ TX POP to AOP modulation loss vs. er (extinction ratio)
α_{TX}	$\triangleq$ TX path intrinsic loss at modulator bias point
p_{TX}	$\triangleq$ TX total output AOP
α_{SMF}	$\triangleq$ Link total power loss (connectors, SMF, other passives)
p_{RX}	$\triangleq$ RX total input AOP
α_{RX}	$\triangleq$ RX path intrinsic loss
p_{PD}	$\triangleq$ RX PD input AOP
r_{PD}	$\triangleq$ RX PD responsivity
α_{AVG}	$\triangleq$ PD AOP to average electrical signal power loss vs. er

Direct Detection (DD) SNR

$i_{\text{SIG}} \triangleq$ RX PD signal current

$$i_{\text{SIG}} = \alpha_{\text{AVG}} r_{\text{PD}} p_{\text{PD}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{TX}} \alpha_{\text{AOP}} r_{\text{PD}} p_0$$

$i_{\text{N}} \triangleq$ RX input referred noise current; all sources

$i_0 \triangleq$ RX input noise current density reference

$\alpha_{\text{N}} \triangleq$ RX input noise current loss vs. i_0

$\text{BW} \triangleq$ RX input noise bandwidth

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

$$\text{snr} = (i_{\text{SIG}} / i_{\text{N}})^2$$

$$\sqrt{\text{snr}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{TX}} \alpha_{\text{AOP}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

Coherent (CH) Signal Path Variables

p_0	$\triangleq$ Input POP (Peak Optical Power) reference
α_{TEC}	$\triangleq$ Input POP loss due to laser TEC current
α_{LS}	$\triangleq$ TX input POP loss due to $(1 - \alpha_{\text{LS}})$ LO (Local Oscillator) input split
$p_{\text{IN-TX}}$	$\triangleq$ TX input POP = AOP since CW
α_{AOP}	$\triangleq$ TX POP to AOP modulation loss vs. MD (mod. drive)
α_{TX}	$\triangleq$ TX path intrinsic loss at modulator bias point
α_{G}	$\triangleq$ TX optical gain ($\alpha_{\text{G}} = 1$ if no amplification)
p_{TX}	$\triangleq$ TX total output AOP
α_{SMF}	$\triangleq$ Link total power loss (connectors, SMF, other passives)

Coherent (CH) Signal Path Variables, cont.

p_{RX}	$\triangleq$ RX total input AOP
p_{LO}	$\triangleq$ RX LO input AOP
$\Phi(t)$	$\triangleq$ Phase angle between p_{RX} and p_{LO} electric fields
α_{RX}	$\triangleq$ RX SIG path intrinsic loss
α_{LO}	$\triangleq$ RX LO path intrinsic loss
p_{PD}	$\triangleq$ RX PD input AOP
r_{PD}	$\triangleq$ RX PD responsivity
α_{AVG}	$\triangleq$ PD AOP to average electrical signal power loss vs. MD

Coherent Signal Addition

Optical signals, with same polarization state, add in the electric field domain

$$\begin{aligned}E_{LO} / \sqrt{Z} &\triangleq \sqrt{p_{LO}} \\E_{RX} / \sqrt{Z} &= \cos \Phi(t) \sqrt{p_{RX}} + j \sin \Phi(t) \sqrt{p_{RX}} \\E_{PD} / \sqrt{Z} &= \sqrt{p_{LO}} + \cos \Phi(t) \sqrt{p_{RX}} + j \sin \Phi(t) \sqrt{p_{RX}} \\P_{PD} &= (\sqrt{p_{LO}} + \cos \Phi(t) \sqrt{p_{RX}})^2 + (\sin \Phi(t) \sqrt{p_{RX}})^2 \\&= p_{LO} + 2 \sqrt{p_{LO}} \sqrt{p_{RX}} \cos \Phi(t) + p_{RX} \\p_{RX} &\ll 2 \sqrt{p_{LO}} \sqrt{p_{RX}} \cos \Phi(t) \\p_{LO} \text{ RIN} &\ll 2 \sqrt{p_{LO}} \sqrt{p_{RX}} \cos \Phi(t) \\p_{PD} &= 2 \sqrt{(p_{LO} p_{RX})} \cos \Phi(t)\end{aligned}$$

Coherent (CH) SNR

$i_{\text{SIG}} \triangleq$ RX balanced PD pair signal current

$$i_{\text{SIG}} = \alpha_{\text{AVG}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})} \cos \Phi(t)$$

$$\cos \Phi(t) \triangleq 1 \quad \alpha_{\text{LS}} \triangleq 1/2 \quad \alpha_{\text{LO}} \triangleq \alpha_{\text{RX}}$$

$$i_{\text{SIG}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}})} \alpha_{\text{TEC}} r_{\text{PD}} p_0$$

$i_{\text{N}} \triangleq$ RX input referred noise current; all sources

$i_0 \triangleq$ RX input noise current density reference

$\alpha_{\text{N}} \triangleq$ RX input noise current loss vs. i_0

$\text{BW} \triangleq$ RX input noise bandwidth

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

$$\text{snr} = (i_{\text{SIG}} / i_{\text{N}})^2$$

$$\sqrt{\text{snr}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}})} \alpha_{\text{TEC}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

Ratio DD SNR to CH SNR: $\sqrt{(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})}$

$$\sqrt{\text{snr}_{\text{DD}}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{TX}} \alpha_{\text{AOP}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

$$\sqrt{\text{snr}_{\text{CH}}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}})} \alpha_{\text{TEC}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

$$r_{\text{PD-DD}} \triangleq r_{\text{PD-CH}}$$

$$\text{BW}_{\text{DD}} \triangleq \text{BW}_{\text{CH}}$$

$$\begin{aligned} \sqrt{(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})} &= \alpha_{\text{AVG-DD}} \alpha_{\text{RX-DD}} \alpha_{\text{SMF}} \alpha_{\text{TX-DD}} \alpha_{\text{AOP-DD}} \alpha_{\text{N-CH}} \\ &\quad / \alpha_{\text{AVG-CH}} \alpha_{\text{RX-CH}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX-CH}} \alpha_{\text{AOP-CH}})} \alpha_{\text{TEC}} \alpha_{\text{N-DD}} \end{aligned}$$

$$\text{Optical } \Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} \text{ dB}$$

$A \triangleq$ loss in optical -dB

$$A = -10\log_{10}(\alpha)$$

$$\Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} = 10\log_{10}(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})$$

$$\begin{aligned} \Delta\text{SNR}_{\text{DD-CH}} / 2 = & - (A_{\text{AOP-DD}} + A_{\text{TX-DD}} + A_{\text{SMF}}) \\ & + (A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + A_{\text{SMF}}) / 2 + A_{\text{TEC}} \\ & - (A_{\text{AVG-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}) \\ & + (A_{\text{AVG-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}) \end{aligned}$$

$$A_{\text{TX-T-DD}} = A_{\text{AOP-DD}} + A_{\text{TX-DD}}$$

$$A_{\text{RX-T-DD}} = A_{\text{AVG-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}$$

$$A_{\text{TX-T-CH}} = A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + 2A_{\text{TEC}}$$

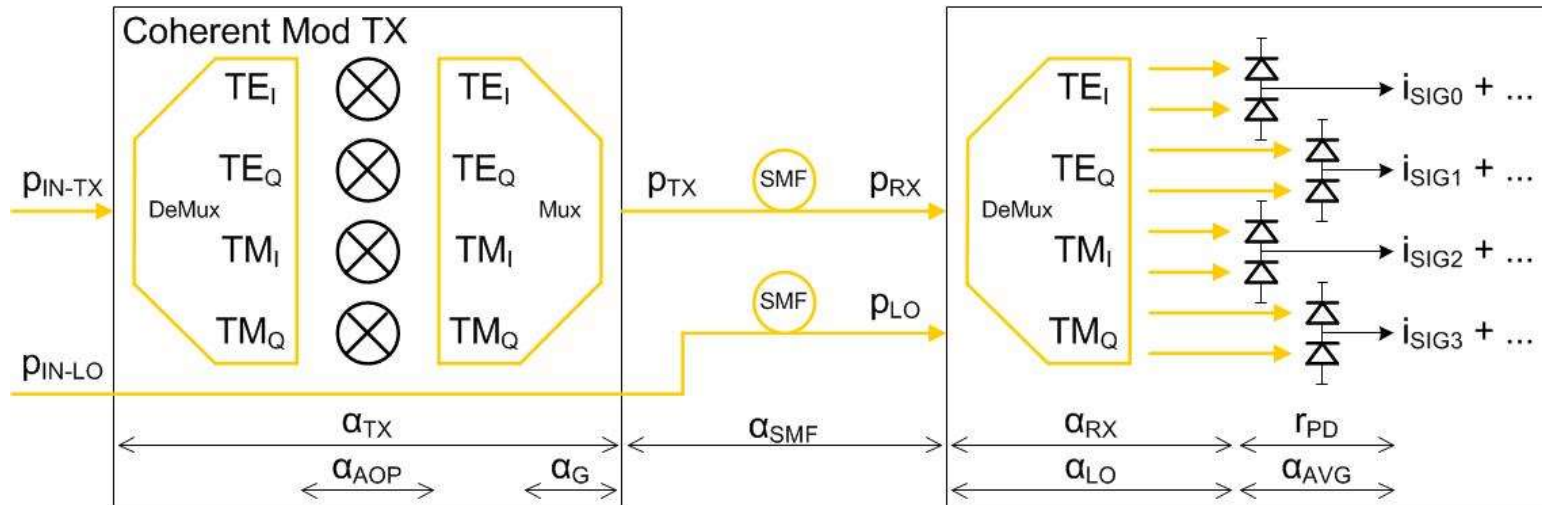
$$A_{\text{RX-T-CH}} = A_{\text{AVG-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}$$

$$\Delta\text{SNR}_{\text{DD-CH}} = (A_{\text{TX-T-CH}} + A_{\text{SMF}} + 2A_{\text{RX-T-CH}}) - 2(A_{\text{TX-T-DD}} + A_{\text{SMF}} - A_{\text{RX-T-DD}})$$

Outline

- NRZ vs HOM
- Serial vs WDM
- Coherent in Telecom
- Coherent in Datacom
- IMDD vs Coherent SNR
- Intra Datacenter Optics
- **Appendix 2**

Coherent (CH) w/ same TX Signal & LO Path



$$p_{\text{IN-TX}} = 4 \alpha_{\text{LS}} \alpha_{\text{TEC}} p_0$$

$$p_{\text{TX}} = \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}} p_{\text{IN-TX}}$$

$$p_{\text{IN-LO}} = 4 (1 - \alpha_{\text{LS}}) \alpha_{\text{TEC}} p_0$$

$$i_{\text{SIG}} = \alpha_{\text{AVG}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})}$$

$$p_{\text{RX}} = \alpha_{\text{SMF}} \alpha_{\text{TX}}$$

$$p_{\text{PD-RX}} = \alpha_{\text{RX}} p_{\text{RX}} / 4$$

$$p_{\text{PD-LO}} = \alpha_{\text{LO}} \alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}} p_{\text{IN-LO}} / 4$$

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

Coherent (CH) RX Signal w/ same TX Signal & LO Path

$i_{\text{SIG}} \triangleq$ RX balanced PD pair signal current

$$i_{\text{SIG}} = \alpha_{\text{AVG}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})}$$

$$\alpha_{\text{LS}} \triangleq 1/2 \quad \alpha_{\text{LO}} \triangleq \alpha_{\text{RX}}$$

$$i_{\text{SIG}} = \alpha_{\text{AVG}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{TX}} \alpha_{\text{AOP}} \alpha_{\text{TEC}} r_{\text{PD}} p_0$$

Equal DD and CH total input AOP condition:

$$p_{\text{IN-DD-TX}} \triangleq p_{\text{IN-CH-TX}} + p_{\text{IN-CH-LO}}$$

$$i_{\text{DD-SIG}} = i_{\text{CH-SIG}}$$

When the LO is remote, i.e. it's a RO, there is no Coherent signal gain!

Same TX Signal and LO Path analysis approach proposed by Mike Frankel, Ciena, 18 Jan 2018.

Outline

- NRZ vs HOM
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- Coherent in Telecom
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- IMDD vs Coherent SNR
- Intra Datacenter Optics
- **Appendix 3**

$$\Delta \text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} \text{ Examples}$$

$$\Delta \text{SNR}_{\text{DD-CH}} / 2 =$$

- $A_{\text{AOP-DD}}$	+ $A_{\text{AOP-CH}} / 2$	// TX
- $A_{\text{TX-DD}}$	+ $A_{\text{TX-CH}} / 2$	// TX
- $(-A_{\text{G}} / 2)$	+ A_{TEC}	// TX Scenario
- A_{SMF}	+ $A_{\text{SMF}} / 2$	// Link
- $A_{\text{RX-DD}}$	+ $A_{\text{RX-CH}}$	// RX
- $A_{\text{AVG-DD}}$	+ $A_{\text{AVG-CH}}$	// RX
- $(-A_{\text{N-DD}})$	+ $(-A_{\text{N-CH}})$	// RX

TX Modulation Loss

- $\alpha_{\text{AOP}}, A_{\text{AOP}} \triangleq$ TX input POP to AOP modulation loss; linear, -dB
- $\alpha_{\text{AOP-NRZ}} [\text{er}] = (\text{er} + 1) / (2 \text{ er})$ // Mod. TX
- $\alpha_{\text{AOP-NRZ}} [\text{er}] = 1$ // DML TX
- $\alpha_{\text{AOP-PAM4}} [\text{er}] = (\text{er} + 1) / (2 \text{ er})$ // Mod. TX
- $\alpha_{\text{AOP-PAM4}} [\text{er}] = 1$ // DML TX
- $\alpha_{\text{AOP-QPSK}} [2V_{\pi}] = 1$
- $\alpha_{\text{AOP-QPSK}} [V_{\pi}] = 1/2$
- $\alpha_{\text{AOP-QAM16}} [2V_{\pi}] = 5/9$
- $\alpha_{\text{AOP-QAM16}} [V_{\pi}] = 5/18$
- Equal DD & CH TX modulation drive
- $MD_{\text{DD-Max}} \triangleq 1/2 MD_{\text{CH-Max}}$
- $MD_{\text{CH}} = V_{\pi}$

TX Modulation Loss Values

- $A_{\text{AOP}} \triangleq$ TX input POP to AOP modulation loss, -dB

mod. loss variable	ER dB	DD mod. loss value -dB		DD DM loss value -dB	
		NRZ	PAM4	NRZ	PAM4
$A_{\text{AOP-DD}}$	∞	3.0	3.0	0.0	0.0
	7	2.2	2.2	0.0	0.0
	4.8	1.8	1.8	0.0	0.0

mod. loss variable	MD	CH loss value -dB		CH loss value -dB / 2	
		QPSK	QAM16	QPSK	QAM16
$A_{\text{AOP-CH}}$	$2V_{\pi}$	0.0	2.6	0.0	1.3
	V_{π}	3.0	5.6	1.5	2.8

TX Signal Path Intrinsic Loss Values

- $A_{TX} \triangleq$ TX path intrinsic loss, -dB

Ex. #	Implementation	DD loss value -dB	CH loss value -dB
		A_{TX-DD}	A_{TX-CH}
1	Ideal TX & RX, no loss	0	0
2	DD CWDM4 TFF DML TX, RX CH SiP	4	14
3	DD CWDM4 TFF EML TX, RX CH SiP (ECOC'18 WS Example)	5	14
4	DD PSM4 SiP TX & RX CH SiP	6	14
5	DD CWDM4 SiP TX & RX, CH SiP	8	14

TX Scenarios

- $\alpha_{\text{TEC}}, A_{\text{TEC}} \triangleq \text{TX}_{\text{CH}}$ input POP loss, laser TEC current; linear, -dB
- $\alpha_{\text{G}}, A_{\text{G}} \triangleq \text{TX}_{\text{CH}}$ optical gain
 $A_{\text{G}} \text{ TX}_{\text{CH}}$ optical gain = - $A_{\text{G}} \text{ TX}_{\text{DD}}$ optical loss in $\Delta\text{SNR}_{\text{DD-CH}}$ table
- Scenario 1: equal laser DC power (40% efficient CH TEC)
 - $i_{\text{Laser-bias-DD}} \triangleq i_{\text{Laser-bias-CH}} + i_{\text{Laser-TEC-CH}}$
 - $\alpha_{\text{TEC}} \triangleq 0.4$
 - $\alpha_{\text{G}} \triangleq 1$
- Scenario 2: equal TX & LO total input POP (no CH TEC)
 - $p_{\text{IN-TX-DD}} \triangleq p_{\text{IN-TX-CH}} + p_{\text{IN-LO-CH}}$
 - $\alpha_{\text{TEC}} \triangleq 1$
 - $\alpha_{\text{G}} \triangleq 1$

TX Scenarios, cont.

- Scenario 3: equal TX total output AOP (no DC power limit)

$$p_{\text{TX-DD}} \triangleq p_{\text{TX-CH}}$$

$$A_{\text{TX-DD}} + A_{\text{AOP-DD}} = A_{\text{G}} + A_{\text{TX-CH}} + A_{\text{AOP-CH}} + A_{\text{LS}} + A_{\text{TEC}}$$

$$\alpha_{\text{TEC}} \triangleq 1$$

$$A_{\text{TEC}} = 0$$

$$\alpha_{\text{LS}} \triangleq 1/2$$

$$A_{\text{LS}} = 3$$

$$- A_{\text{G}} / 2 = ((A_{\text{TX-CH}} + A_{\text{AOP-CH}} + 3) - (A_{\text{TX-DD}} + A_{\text{AOP-DD}})) / 2$$

TX Scenarios Loss Values

- A_{TEC} $\triangleq$ TX_{CH} input POP loss due to laser TEC current, -dB
- A_{G} $\triangleq$ A_{G} TX_{CH} optical gain = $-A_{\text{G}}$ TX_{DD} optical loss

$\Delta\text{SNR}_{\text{DD-CH}} / 2$ TX Scenario		DD loss variable	DD loss value -dB	CH loss variable	CH loss value -dB
1	Equal laser DC power	$-A_{\text{G}} / 2$	0	A_{TEC}	4
2	Equal total input AOP	$-A_{\text{G}} / 2$	0	A_{TEC}	0
3	Equal TX total output AOP	$-A_{\text{G}} / 2$	formula	A_{TEC}	0

Link Loss Values

- $A_{\text{SMF}} \triangleq$ Link total power loss (connectors, SMF, other passives), -dB
- Standard datacenter link loss budget
 $A_{\text{SMF}} \triangleq 4$

DD loss value -dB	CH loss value -dB
A_{SMF}	$A_{\text{SMF}} / 2$
4.0	2.0

RX Signal Path Intrinsic Loss Values

- $A_{RX} \triangleq$ RX path intrinsic loss, -dB
- $A_{LO} \triangleq$ RX LO path intrinsic loss, -dB: $A_{LO-CH} \triangleq A_{RX-CH}$

Ex. #	Implementation	DD loss value -dB	CH loss value -dB
		A_{RX-DD}	A_{RX-CH}
1	Ideal TX & RX, no loss	0	0
2	DD CWDM4 TFF DML TX, RX CH SiP	2	4
3	DD CWDM4 TFF EML TX, RX CH SiP (ECOC'18 WS Example)	2	4
4	DD PSM4 SiP TX & RX CH SiP	2	4
5	DD CWDM4 SiP TX & RX, CH SiP	4	4

RX Modulation Loss

- $\alpha_{\text{AVG}}, A_{\text{AVG}} \triangleq$ RX PD AOP to average electrical signal power loss; linear, -dB
- $\alpha_{\text{LS}} \triangleq$ TX input POP loss due to $(1 - \alpha_{\text{LS}})$ split with LO input
- $\alpha_{\text{AVG-NRZ}} [\text{er}] = (\text{er} - 1) / (\text{er} + 1)$
 $\alpha_{\text{AVG-PAM4}} [\text{er}] = \sqrt{(5/9)} (\text{er} - 1) / (\text{er} + 1)$
- $\alpha_{\text{AVG-QPSK}} [2V_{\pi}] = 1$
 $\alpha_{\text{AVG-QPSK}} [V_{\pi}] = 1$
 $\alpha_{\text{AVG-QAM16}} [2V_{\pi}] = 1$
 $\alpha_{\text{AVG-QAM16}} [V_{\pi}] = 1$
- Equal DD & CH TX modulation drive
 $\text{MD}_{\text{DD-Max}} \triangleq \frac{1}{2} \text{MD}_{\text{CH-Max}}$
 $\text{MD}_{\text{CH}} = V_{\pi}$

RX Modulation Loss Values

- $A_{AVG} \triangleq$ RX PD AOP to average electrical signal power loss, -dB

Mod. loss variable	ER dB	DD Mod. loss value -dB		DD DM loss value -dB	
		NRZ	PAM4	NRZ	PAM4
A_{AVG-DD}	∞	0.0	1.3	0.0	1.3
	7	1.8	3.0	1.8	3.0
	4.8	3.0	4.3	3.0	4.3

Mod. loss variable	MD	CH loss value -dB	
		QPSK	QAM16
A_{AVG-CH}	$2V_{\pi}$	0.0	0.0
	V_{π}	0.0	0.0

Coherent Unequal SIG/LO Split Loss

- α_{ALS}, A_{ALS} $\triangleq$ Unequal SIG/LO split $\alpha_{LS} \neq 1/2$ loss; linear, -dB
 α_{ALS} $= 2 \sqrt{\alpha_{LS} (1 - \alpha_{LS})}$
 α_{LS} $\triangleq 1/2$
 A_{ALS} $= 0$
 α_{LS} $\triangleq 2/3$
 A_{ALS} $= 0.3$
- A'_{AVG-CH} $= A_{AVG-CH} + A_{ALS}$

mod. loss variable	MD	CH loss value -dB			
		$\alpha_{LS} = 1/2$		$\alpha_{LS} = 2/3$	
		QPSK	QAM16	QPSK	QAM16
A'_{AVG-CH}	$2V_{\pi}$	0.0	0.0	0.3	0.3
	V_{π}	0.0	0.0	0.3	0.3

RX Input Referred Noise Current Loss Values

- A_N $\triangleq$ RX input noise current density loss vs. reference, -dB
- $\alpha_N i_0$ $\triangleq$ RX input noise current density
- RX input noise current density values
 - $\alpha_{N-DD} i_0 = 12\text{pA} / \sqrt{\text{Hz}}$
 - $\alpha_{N-DD} \triangleq 1$
 - $i_0 = 12\text{pA} / \sqrt{\text{Hz}}$
 - $\alpha_{N-CH} i_0 = 20\text{pA} / \sqrt{\text{Hz}}$
 - $\alpha_{N-CH} = 5/3$

DD loss value -dB	CH loss value -dB
A_{N-DD}	A_{N-CH}
0.0	-2.2

Ex.1: $\Delta\text{SNR}_{\text{DD-CH}}/2$ Ideal TX & RX no loss

Ex. 1 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD Ideal TX ER = ∞ loss value -dB		CH loss var.	CH Ideal TX MD = V_{π} loss value -dB	
Loss Type		A_{DD}	NRZ	PAM4	A_{CH}	QPSK	QAM16
TX		A_{AOP}	3.0	3.0	$A_{\text{AOP}}/2$	1.5	2.8
		A_{TX}	0		$A_{\text{TX}}/2$	0	
1	Equal laser DC power	$-A_{\text{G}}/2$	0.0		A_{TEC}	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		1.5	2.8		0.0	
Link		A_{SMF}	4		$A_{\text{SMF}}/2$	2	
RX		A_{RX}	0		A_{RX}	0	
		A_{AVG}	0.0	1.3	A'_{AVG}	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		NRZ - QPSK	PAM4 - QAM16	
2.7	2.7	-1.3	-1.3		-2.8	-4.1	

Ex.2: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD CWDM TFF, DML TX

Ex. 2 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD CWDM4 TFF, DML TX ER = 4.8 loss value -dB		CH loss var.	CH SiP TX MD = V_{π} loss value -dB	
Loss Type		A_{DD}	NRZ	PAM4	A_{CH}	QPSK	QAM16
TX		A_{AOP}	0.0	0.0	$A_{\text{AOP}}/2$	1.5	2.8
		A_{TX}	4		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	$-A_{\text{G}}/2$	0.0		A_{TEC}	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		8.0	9.3		0.0	
Link		A_{SMF}	4		$A_{\text{SMF}}/2$	2	
RX		A_{RX}	2		A_{RX}	4	
		A_{AVG}	3.0	4.3	A'_{AVG}	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		NRZ - QPSK	PAM4 - QAM16	
7.7	7.7	3.7	3.7		-4.3	-5.5	

Ex.3: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD CWDM TFF, EML TX

Ex. 3 (ECOC'18 WS Ex.) $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD CWDM4 TFF, EML TX ER = 7 loss value -dB		CH loss var.	CH SiP TX MD = V_{π} loss value -dB	
Loss Type		A_{DD}	NRZ	PAM4	A_{CH}	QPSK	QAM16
TX		A_{AOP}	2.2	2.2	$A_{\text{AOP}}/2$	1.5	2.8
		A_{TX}	5		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	$-A_{\text{G}}/2$	0.0		A_{TEC}	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		6.4	7.7		0.0	
Link		A_{SMF}	4		$A_{\text{SMF}}/2$	2	
RX		A_{RX}	2		A_{RX}	4	
		A_{AVG}	1.8	3.0	A'_{AVG}	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16
5.7	5.7	1.7	1.7	-4.6	-5.9		

Ex.4: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD PSM4 SiP

Ex. 4 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD PSM4 SiP TX ER = 7 loss value -dB		CH loss var.	CH SiP TX MD = V_{π} loss value -dB	
Loss Type		A_{DD}	NRZ	PAM4	A_{CH}	QPSK	QAM16
TX		A_{AOP}	2.2	2.2	$A_{\text{AOP}}/2$	1.5	2.8
		A_{TX}	6		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	$-A_{\text{G}}/2$	0.0		A_{TEC}	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		5.9	7.2		0.0	
Link		A_{SMF}	4		$A_{\text{SMF}}/2$	2	
RX		A_{RX}	2		A_{RX}	4	
		A_{AVG}	1.8	3.0	A'_{AVG}	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		NRZ - QPSK	PAM4 - QAM16	
4.7	4.7	0.7	0.7		-5.1	-6.4	

Ex.5: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD CWDM4 SiP

Ex. 5 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD CWDM4 SiP TX ER = 7 loss value -dB		CH loss var.	CH SiP TX MD = V_{π} loss value -dB	
Loss Type		A_{DD}	NRZ	PAM4	A_{CH}	QPSK	QAM16
TX		A_{AOP}	2.2	2.2	$A_{\text{AOP}}/2$	1.5	2.8
		A_{TX}	8		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	$-A_{\text{G}}/2$	0.0		A_{TEC}	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		4.9	6.2		0.0	
Link		A_{SMF}	4		$A_{\text{SMF}}/2$	2	
RX		A_{RX}	4		A_{RX}	4	
		A_{AVG}	1.8	3.0	A'_{AVG}	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		NRZ - QPSK	PAM4 - QAM16	
0.7	0.7	-3.3	-3.3		-8.1	-9.4	

$\Delta\text{SNR}_{\text{DD-CH}}$ dB Examples, 4dB SMF Link

$\Delta\text{SNR}_{\text{DD-CH}}$ dB		Scenario		1. Equal laser DC power		2. Equal total input AOP		3. Equal TX output AOP	
Ex. #	TX & RX Implementation	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16
1	Ideal TX & RX no loss DD ER = ∞ , CH MD = V_{π}	5.4		-2.6		-5.6		-8.1	
2	DD CWDM4 TFF DML TX ER = 4.8, SiP CH MD = V_{π}	15.4		7.4		-8.6		-11.1	
3	DD CWDM4 TFF EML TX ER = 7, SiP CH MD = V_{π}	11.5		3.5		-9.3		-11.8	
4	DD PSM4 SiP TX ER = 7, SiP CH MD = V_{π}	9.5		1.5		-10.3		-12.8	
5	DD CWDM4 SiP TX ER = 7, SiP CH MD = V_{π}	1.5		-6.5		-16.3		-18.8	

Coherent vs. IMDD SNR Examples Conclusion

Application	Direct Detection NRZ / PAM4 SNR		SNR Relation	Coherent QPSK / QAM16 SNR	
	TX	RX		TX	RX
Laser DC Power Constrained	EML, DML single λ or TFF, PLC WDM	PIN single λ or TFF, PLC WDM	$\gg$	SiP	SiP
	single λ SiP (PSM)	single λ SiP (PSM)	$\gg$	SiP	SiP
4dB Link Loss	WDM SiP	WDM SiP	$\approx$	SiP	SiP
TX Out Power Constrained	Any	PIN	$\ll$	SiP	SiP

For most intra datacenter links, IMDD has better SNR than Coherent, contrary to conventional wisdom.

IMDD vs Coherent Appendices

Thank You

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